### High Fines Content Beach Placement Project Case Studies Florida and Texas

**Empirical Formula to Estimate Borrow Sediment Ultimate Capability** 

#### By Coraggio Maglio, P.E. CFM & Dr. Himangshu Das, PE

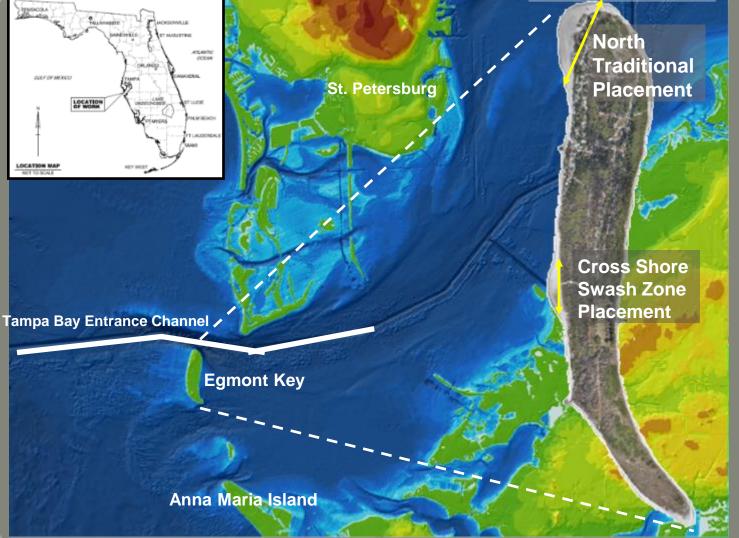
US Army Corps Galveston Branch Chief H&H 9 Feb 2018

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# **EGMONT KEY 2014/5**

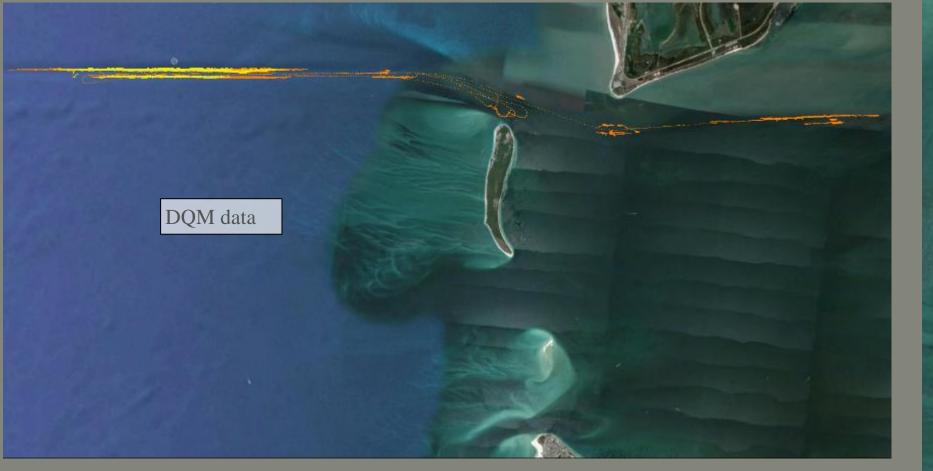


- Two placements
  - 320K CY placed
  - 107 CY placed
- +20% passing 230
- Sediment monitoring
  - Grain Size
  - Color
  - Compaction





### **2014/5 DREDGING AND PLACEMENT**



UAV flight aerial 16 March 2015

Cross Shore Swash Zone Placement

107K cy placed

### **FINES CONTENT**

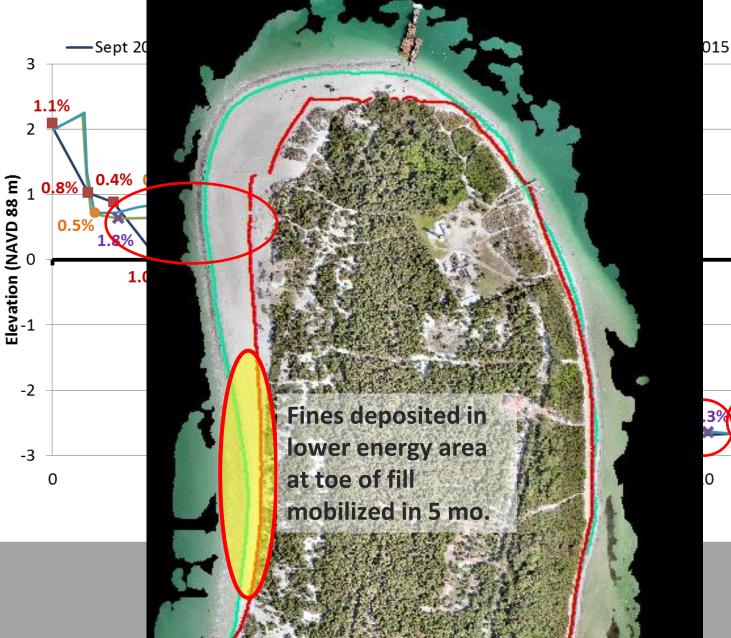
| Tampa Harbor MD - Egmont Key 2014 |         |                   |  |  |  |  |  |  |  |
|-----------------------------------|---------|-------------------|--|--|--|--|--|--|--|
|                                   | # of    | Avg. % by wt.     |  |  |  |  |  |  |  |
|                                   | Samples | passing 230 sieve |  |  |  |  |  |  |  |
| In-situ avg.                      | 80      | 20.7              |  |  |  |  |  |  |  |
| In-situ Traditional               | 45      | 20*               |  |  |  |  |  |  |  |
| In-situ CSSZ                      | 35      | 24*               |  |  |  |  |  |  |  |
| Pre-Beach                         | 6       | 0.03              |  |  |  |  |  |  |  |
| Post-Dredged avg.                 | 21      | 0.51**            |  |  |  |  |  |  |  |
| Post Traditional                  | 14      | 0.52**            |  |  |  |  |  |  |  |
| PostCSSZ                          | 7       | 0.49**            |  |  |  |  |  |  |  |

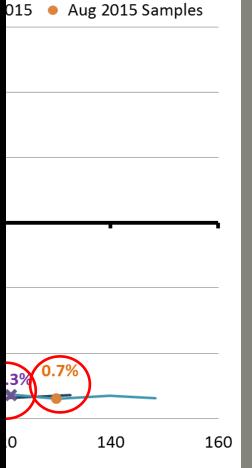
\* Based on DQM and core boring data

\*\*Sampling occurred within 72 hours of placement completion



# WHERE DID THE FINES GO?



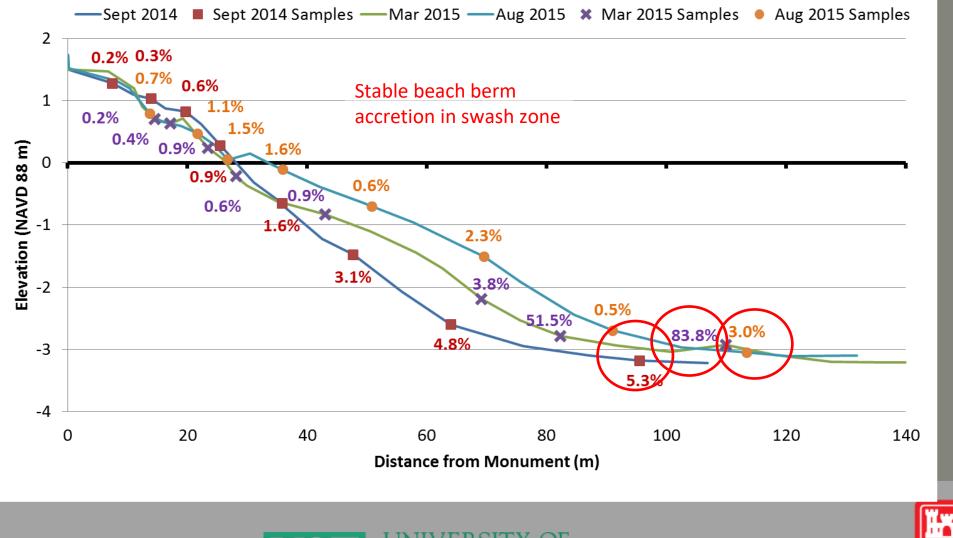






# **CCSZ PLACED FINES?**

#### **R10** Profiles with % Fines







### WHAT ABOUT COMPACTION?

| USF Line 17    |              |       | and the second s |         | one<br>ometer | 32 <sup>29</sup> 21<br>10 11<br>4<br>12<br>5 13<br>14<br>14<br>12<br>5<br>14<br>14<br>14<br>15<br>6<br>17<br>6<br>18 | V2V205<br>1<br>3<br>7<br>4<br>5<br>7<br>4<br>5<br>7<br>7<br>8<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10 | 1-Construction Cove Penderorm<br>(*-(*) - (*-12) 12'-16'<br>200 Refutual<br>500 Refutual<br>500 Refutual<br>500 Refutual<br>500 Refutual<br>500 Selutas<br>500 Selut |        |         |
|----------------|--------------|-------|--|---------|---------------|--|---|--|--------|---------|
| USF Line 6 -10 | Depth (in)   | 0"-6" | 6"-12"   | 12"-18" |               |  | Depth (in)  | 0"-6"  | 6"-12" | 12"-18" |
|                | Min (psi)    | 100   | 100  | 198     |               |  | Min (psi)   | 50   | 125    | 200     |
| USF Line 4     | Max (psi)    | 580   | 700  | 617     |               |  | Max (psi)   | 600  | 700    | 600     |
| A CONTRACTOR   | Avg (psi)    | 293   | 406  | 457     |               |  | Avg (psi)   | 328  | 482    | 436     |
|                | Median (psi) | 295   | 431  | 515     |               |  | Median (psi)  |  | 500    | 500     |
|                | # samples    | 19    | 19   | 19      |               |  | # samples   | 21   | 21     | 21      |
|                | Refusals     | 1     | 4  | 5       |               | the second second  | Refusals  | 3  | 6      | 10      |
|                | % Refusal    | 5%    | 21%  | 26%     |               |  | % Refusal   | 14%  | 29%    | 48%     |

Increase in refusals due to shell hash areas





#### WHAT ABOUT COLOR?

| Tampa Harbor I | MD - Egmon | t Key 2014 |  |
|----------------|------------|------------|--|
|                | # of       | Value      |  |
|                | Samples    | avg.       | State Stat |
| In-situ        | 80         | 4.36*      |  |
| pre-Beach      | 13         | 5.9        |  |
| post-Dredged   | 24         | 5.3        |  |
| Traditional    | 16         | 5.0        |  |
| CSSZ           | 8          | 5.9        |  |
|                |            |            |  |

\*Measurements made with chart. Munsell color value<5 unacceptable for beach placement in Florida NOTES: Triplicate measurements of hue, value, and chroma were collected from three areas on each moist sand sample using a digital colorimeter (CR-400, Konica Minolta, Osaka, Japan).





# **GALVESTON BENEFICIAL USE 2015/6**

Galveston Channel: 9.7%-99.5% fines
 Average: 38.1% fines
 Post-fill: 1.14% fines
 Minimal longitudinal dike used to capture placed materials basically CSSZ placement





94 samples collected on the dredge Terrapin Island – 2 loads

- 35 Inflow
- 59 overflow

330 samples collected at the beach over 3 months by GLDD

- Discharge slurry
- Carrier water
- Beach berm





#### **BABE'S BEACH 2015/6**

January 2017 ~ 1yr Post Placement

January 2014

#### Legend **Babes Beach Babes Beach** egend Babes Beach between 61st and 75th Street post placement Babes Beach between 61st and 75th Street Pre Placment (2014) Google Earth Google Earth N image © 2016 OlgitalGiobe 1000 ft 1000 ft 3 2016 Google





### BABE'S BEACH 2015/6







### **GALVESTON BENEFICIAL USE 2015/6**

#### 2015 Galveston Seawall Beach Expansion

Great Lakes' Galveston Beach Surveys

Survey data was collected the the on-site contractor.

**Beach Elevation** 

S < 0</p>
S 0 - 2
S 2 - 4
S 4 - 6
S 6 - 8.5

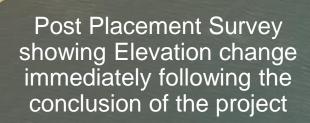
The first survey, which covers the first 1200ft from the 61st Pier, was collected in late September / Early October (Actual date unknown).

1.000

1,250

The second survey runs from 1200ft to 3200ft and was collected 16 October.

The last survey taken was from 3200ft to 4900ft and was collected on 18 November.

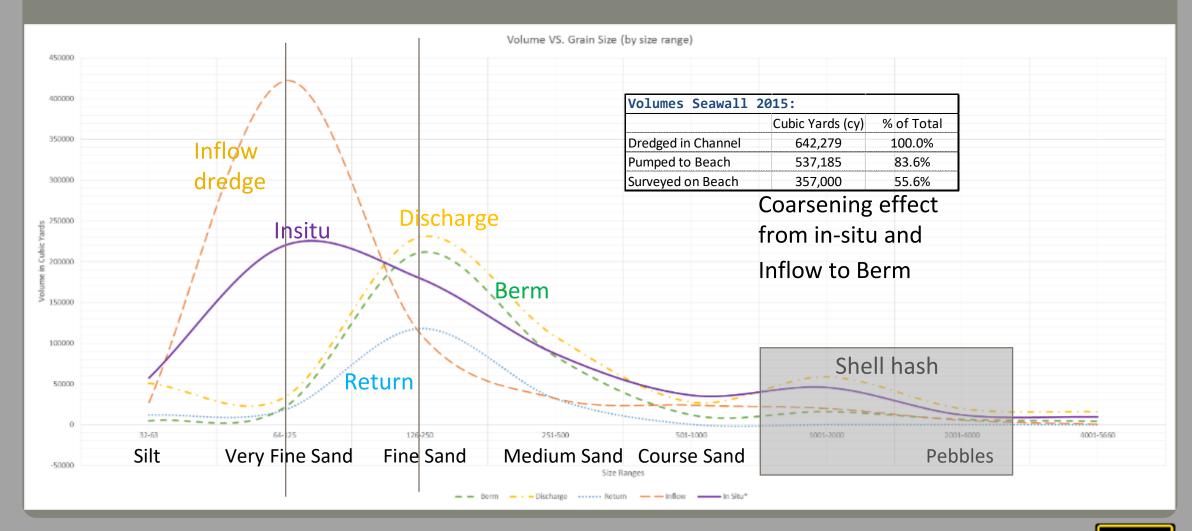








### **GALVESTON BENEFICIAL USE 2015/6**







# CONE PENETROMETER DATA

|              |        |         |              | Pre-Fill |     |              |                 | Section of the sectio |           |
|--------------|--------|---------|--------------|----------|-----|--------------|-----------------|--|-----------|
|              |        |         |              | Pre-Fill | _   | _            |                 |  |           |
|              |        |         | Depth in     |          |     |              |                 | and the second second  |           |
|              |        |         | inches       | 0-6"     | 6-  | -12″         |                 | and the second   |           |
|              |        |         | Min (PSI)    | 350      | 400 | )            |                 |  |           |
|              |        |         | Max (PSI)    | 600      | 650 | )            |                 |  |           |
|              |        |         | Avg (PSI)    | 475      | 525 | 5            |                 | Automation in the  |           |
|              |        |         | Median       | 475      | 525 | 5            |                 |  |           |
|              |        |         | # of Samples | 6        | 6   |              |                 |  |           |
|              |        |         | Refusals     | 0        | 2   |              |                 | and the second sec   |           |
|              | Pos    | st Fill | % Refusals   | 0%       | 33% | 6 Post Fil   | l that has beei | n reworked in  | the swash |
| Depth in     |        |         |              |          |     | Depth in     |                 |  |           |
| inches       | 0-6″   | 6-12″   | 12-18″       |          |     | inches       | 0-6″            | 6-12"  | 12-18″    |
| Min (PSI)    | 100    | 400     | 450          |          |     | Min (PSI)    | 400             | 550  | 600       |
| Max (PSI)    | 600    | 750     | 700          |          |     | Max (PSI)    | 450             | 600  | 700       |
| Avg (PSI)    | 386.11 | 538.46  | 590          |          |     | Avg (PSI)    | 425             | 575  | 650       |
| Median       | 350    | 575     | 575          |          |     | Median       | 425             | 575  | 650       |
| # of Samples | 21     | 23      | 9            |          |     | # of Samples | 2               | 2  | 2         |
| Refusals     | 3      | 5       | 4            |          |     | Refusals     | 0               | 0  | 0         |
| % Refusals   | 14%    | 22%     | 44%          |          |     | % Refusals   | 0%              | 0%   | 0%        |

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#### WHAT ABOUT THE COLOR?

|                           | Hue   | Value | Chroma |
|---------------------------|-------|-------|--------|
| Inflow Grab Sample        | 2.25  | 3.28  | 1.52   |
| Overflow Grab Sample      | 2.46  | 3.02  | 1.59   |
| Pre-Fill Berm/Swash/Dune  | 17.61 | 3.96  | 1.63   |
| Post Fill Berm/Swash/Dune | 5.18  | 4.15  | 1.77   |
| Total Change              | 2.93  | 0.87  | 0.25   |

- Because 71% of insitu sediment is quartz sand
- project experienced lightening effect and color change
- due to the loss of fines during the dredging and placement process.





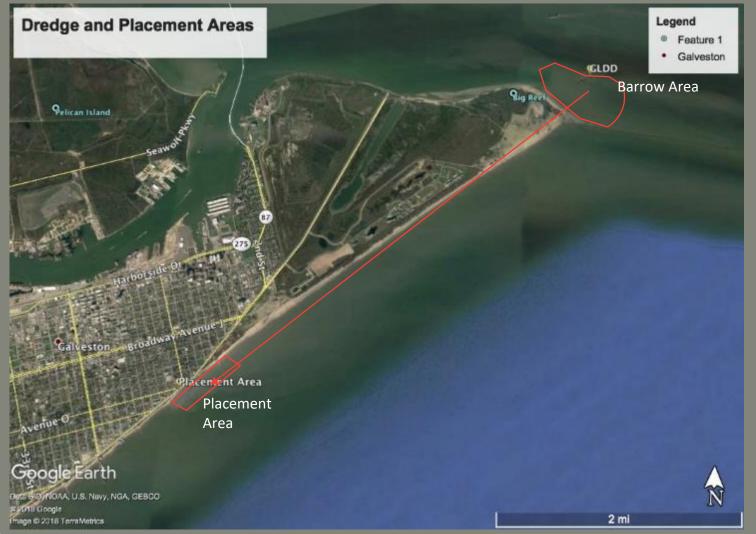


#### GALVESTON, TX 2016

#### EGMONT KEY, FL 2015

| Phase ID (6)                        | Chemical Formula                   | PDF-#   | NA      | NR      | NP     | Wt% (esd)        | RIR                   | Phase (D (E)  | Chemical Formula   | PDF-#  | NA     | NR             | NP | Will (and                | RIR           |
|-------------------------------------|------------------------------------|---|---------|---------|--------|------------------|-----------------------|---|--|--|--------|----------------|----|--------------------------|---------------|
| Albite (heat-treated)               | Na(AISi3O8)                        | 01-089-6429   |         | 114     | -4     | 8.5 (0.2)        | 0.64                  | Phase (D (6)<br>Calcite   |  | 01-083-0577  | TAPA   | 12             | T1 | Wt% (esd)                |               |
| Aragonite                           | Ca(CO3)                            | 01-075-2230   |         | 33      |        | 6 1 0.17         | n. 14                 | 1 leroc nei h V mum   | Ca(CO3)<br>KAISi3O8  | 01-076-0918  |        | 113            | 10 | 12.5 (0.1)<br>3.0 (0.1)  |               |
| Calcite                             | Ca(CO3)                            | 01-083-0577   |         | 12      | 8      | 9 0.13           |                       | I LIDE NO N V MILIN   | KMg3AISi3O10OHF  | 01-078-0918  |        | 107            | 3  | 0.0 (0.0)                |               |
| Calcite magnesian                   | (Mg.129Ca.871)(CO3)                | 01-086-2336   |         | 12      | 3      | 0.6 (0.1)        |                       | Araponite   | Ca(CO3)  | 01-075-2230  |        | 33             | 12 | 33.3 (0.2)               |               |
| Acrocline maximum                   | KAISI308                           | 01-076-0918   |         | 113     | 12     | 6.8 (0.1)        | 0.60                  | Quartz  | SIO2   | 01-085-0794  |        | 12             | 11 | 48.5 (0.3)               |               |
| Quartz                              | SiO2                               | 01-085-0794   |         | 12      | 11     | 71.1 (0.3)       | 3.11                  | Calcite magnesian   | (Mg.129Ca.871)(CO3)  | 01-086-2336  |        | 12             | 4  | 2.7 (0.2)                |               |
|                                     | XRF(WI%): CaO=7.6%, I              | K2O=1.1%, SiO2=81.3%,   | AI2O3=2 | .9%, Mg | O=0.0% | Na2O=1.0%, CC    | 02=6.0%               | Construction of the second  | THE REPORT OF A DESCRIPTION OF A DESCRIP | CaO=27.0%, K2O=0.5%, S   |        |                |    | The second second second |               |
| lefinement Converged (R/E)          | =1.62), + Round=4, Iter=6, P=56, R | *5.32% (E+3.29%, EPS+)  | ).5)    |         |        |                  |                       | Refinement Converged (R/E-  | =1.45). + Round=4, Itar=4, P=62, R   | =5.35% (E=3.70%, EPS=  | 0.5)   |                |    |                          |               |
| R-5.5%<br>2-5.2%<br>3-5.2%          |                                    | Quartz • SiO2<br>Albite (heat-treated) •<br>Calcite • Ca(CO3)<br>Microcline maximum •<br>Aregonite • Ca(CO3)<br>Calcite magnesian • ( | KAISi3  | 08      | (C     |                  | Ountz                 | R-57%<br>2-52%<br>3-52%   | 11.00 100<br>527- 12.94  | Quartz • SiO2<br>Aragonite • Ca(CO3)<br>Calcite • Ca(CO3)<br>Microcline maximum<br>Calcite magnesian •<br>Biotite • KMg3AlSi3O | KAISI3 | 08<br>Ca 871)( | C  | Angement                 | Quartz System |
| 75-<br>75-<br>751 / Josephile<br>80 | rerged (R/E=1.62)                  |   |         |         |        |                  | and the second second | 100<br>100<br>77-<br>75) Attaunut<br>50-  | erged (R/E=1.45)   | *  |        |                |    |                          |               |
| Calote + Ca(CO3)                    | Negalsbog in the inter-            | ()<br>()<br>()<br>()<br>()<br>()<br>()<br>()<br>()<br>()  | 8       | 25      |        | 8- = = = +1.744Å | 1                     | Calcos + CalCos<br>Guartz + SO2<br>Amponter + CalCos<br>Calcos + CalCos<br>Microsine meximu<br>Calcos + KMa3A(S<br>To | <u> </u>   | 210  | ulalu  | 82             |    | 8 5 1875A                | E 1 671A      |

### **GALVESTON 2017 NOURISHMENT**



RS Weeks 30" Cutter Suction Dredge

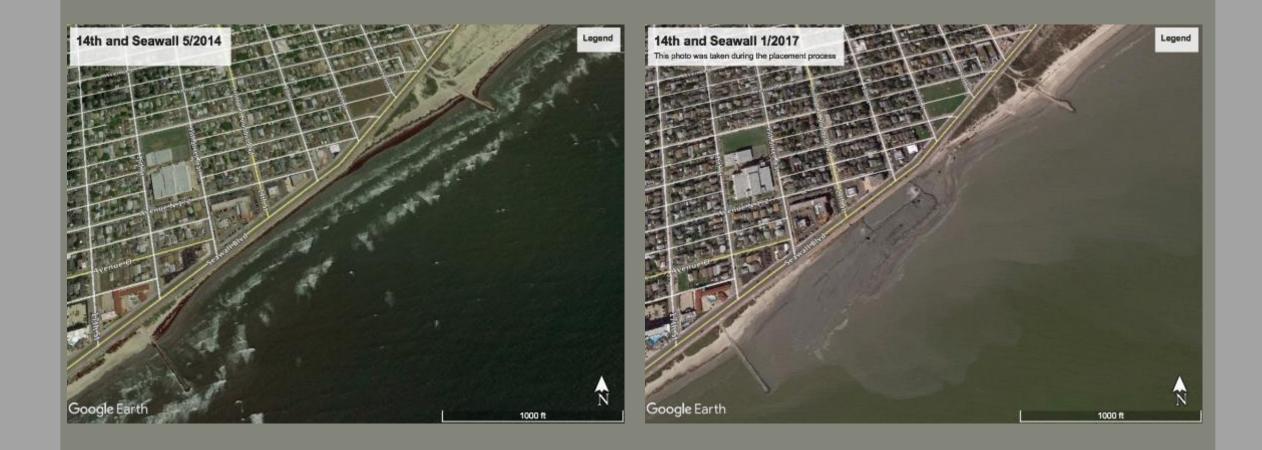


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### **GALVESTON NOURISHMENT 2017 – AERIAL**







### GALVESTON NOURISHMENT 2017 - OPERATIONS

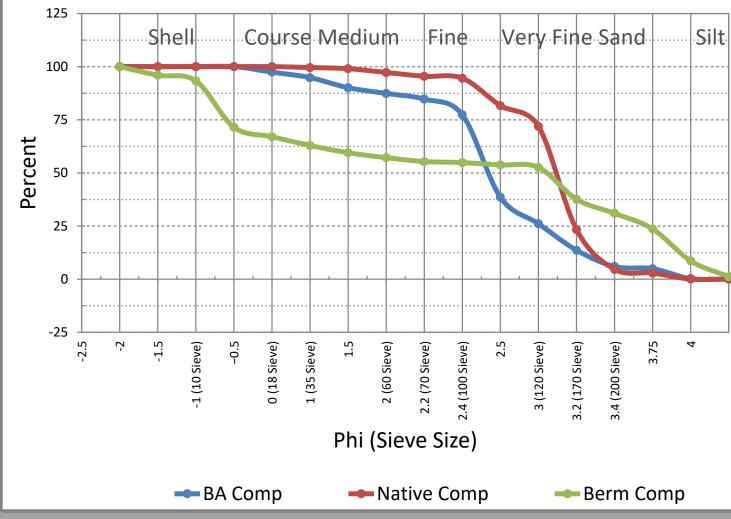






### **GALVESTON 2017 – GRAIN SIZE**

Grain Size Distribution Gal. 2017



| Galveston Seawall Beach Nourishment 2017 |               |                     |  |  |  |  |  |  |
|--|---------------|---------------------|--|--|--|--|--|--|
| Material Source                          | D50 (mm)      | % Fines (200 Sieve) |  |  |  |  |  |  |
| Native Beach Sand                        | 0.14*         | 2.9*                |  |  |  |  |  |  |
| South Jetty Borrow Area                  | 0.16*         | 9.2*                |  |  |  |  |  |  |
| Post-Fill Samples                        | 0.15          | 8.6                 |  |  |  |  |  |  |
| * data from HDR Design I                 | Memo dated 30 | ) Nov 2015          |  |  |  |  |  |  |

Finer sediment was trapped in the fill during the placement event primarily due to methodology

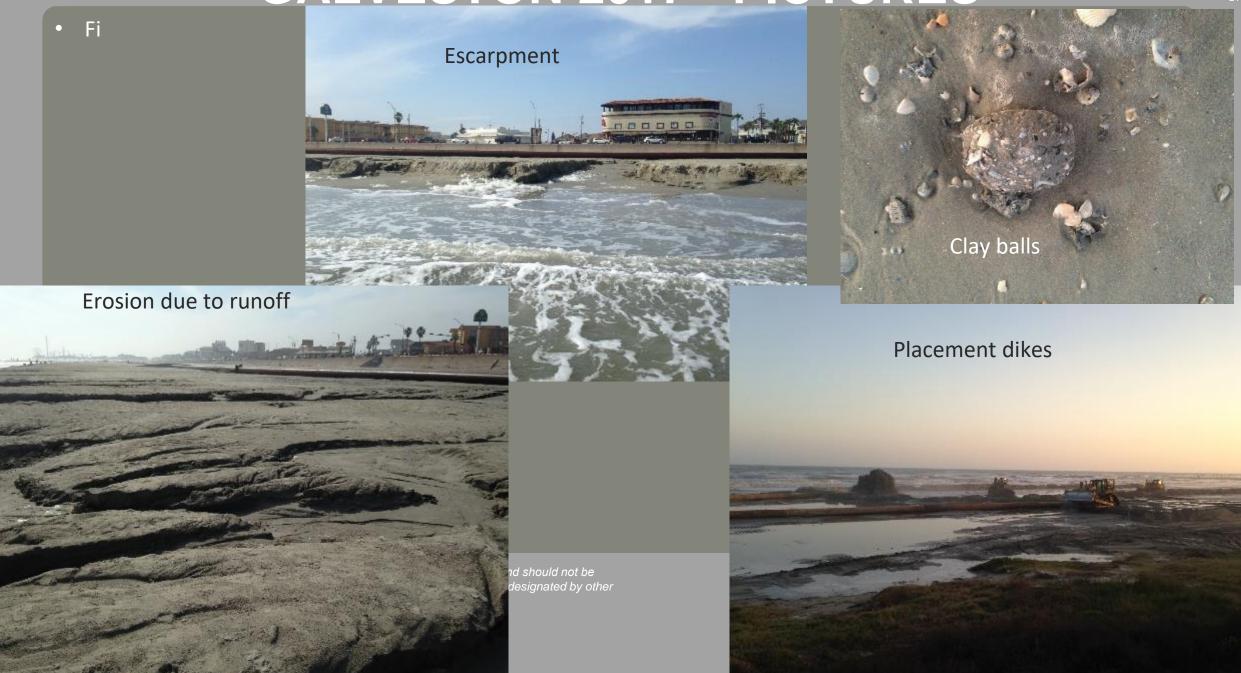




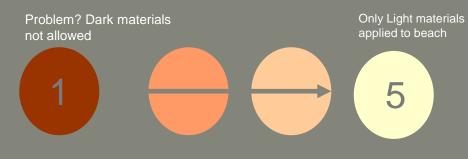


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# **GALVESTON 2017 - PICTURES**



### APPLIED R&D – MUNSELL COLOR COLOR CHANGE PROPENSITY



- Bulk color is due to:
  - % Dark minerals
  - Staining
  - % Dark Organics
- Sediment Color Change is due to:
  - Bleaching
  - Mixing (Losses)
  - Abrasion

ERDC

R&D by: J. Berkowitz, A. Priestas, C. VanZomeren, Jodi Smith

Journal of Coastal Research 00 0 000-000 Coconut Creek, Florida Month 0000

Potential Color Change Dynamics of Beneficial Use Sediments

Jacob F. Berkowitz\*, Christine M. VanZomeren, Anthony M. Priestas

U.S. Army Corps of Engineers Engineer Research and Development Center Vicksburg, MS 39180, U.S.A.

ABSTRACT



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Berkowitz, J.F.; VanZomeren, C.M., and Priestas, A.M., 0000. Potential color change dynamics of beneficial use sediments. *Journal of Constal Research*, 00(0), 000–000. Coconut Creek (Florida), ISSN 0749-0208.

Soliment color is important in determining aesthetic and habitat auitability for beach neurishment projects; however, aedimant derived from dredging operations must meet locally established color compatibility requirements (*i.e.* cannot be to dark). Often, potential sediment sources are close to meeting specified thresholds, and previous observations suggest that aediments may lighten over time following bach nourishment. This work seeks to characterize the degree of color change potential based on the removal of constituents affecting sediment color. Thus, a sequential chanical treatment was developed to examine color changes associated with the removal of carbonates, org anic matter, and iron oxide coatings from aediments collected from eight U.S. Army Corps of Engineers dredging operations. The results show that Munsell values increased by an average of 1.0 unit (became lighter in color) upon removal of these secondary constituents. In addition, five of the eight aediments examined surpassed established color, and high capacity findings suggest that sediments with initially unacceptable color, and high cooler change, may increase potential use of limited sediment resources. Puture work will further relate color shifts to sediment mixing, and solar blacked ing realized color changes under real-world second

ADDITIONAL INDEX WORDS: Sediment color, Munsell color, beach nourishment, beneficial use.

#### INTRODUCTION

Color compatibility between dredged and native beach

and number notation (e.g., 5YR 5/6). Hue designations include red (R), yellow (Y), neutral (N), green (G), blue (B), and number (P). For example, the designation VR refers to the





#### **APPLIED R&D COLOR CHANGE PROPENSITY**

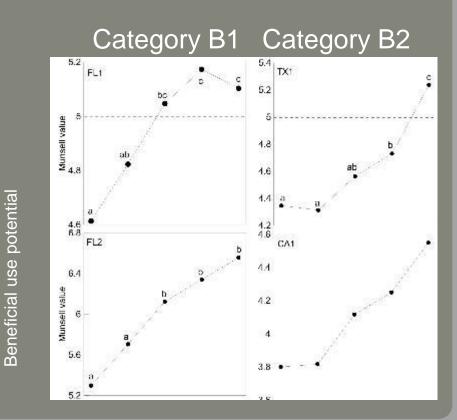
Problem - Dredged material color limits BU due to agency regarding turtle nesting and habitat concerns, etc.

Objectives - Understand sediment color change capacity

- Develop predictive capability for color change to promote BU

Category A - meets criteria in un-treated condition Category B1 - potential for rapid color change Category B2 - potential for color change over time Category C - low potential for color change

|                   |        |           |          |         |          |          |         |         | <u>.</u> |
|-------------------|--------|-----------|----------|---------|----------|----------|---------|---------|----------|
|                   | MD1 Ca | ategory A | FL1 Cate | gory B1 | AL1 Cate | egory B2 | CA1 Cat | egory C |          |
| Treatment         | Value  | Chroma    | Value    | Chroma  | Value    | Chroma   | Value   | Chroma  | ]        |
| Untreated         |        |           | Х        |         | х        | Х        | х       |         |          |
| Carbonates        |        |           | Х        |         | Х        | х        | Х       |         |          |
| Organic<br>matter |        |           |          |         | x        | Х        | х       |         |          |
| Amorphous<br>Fe   |        |           |          |         |          |          | х       |         |          |
| Crystalline Fe    |        |           |          |         |          |          | Х       |         |          |



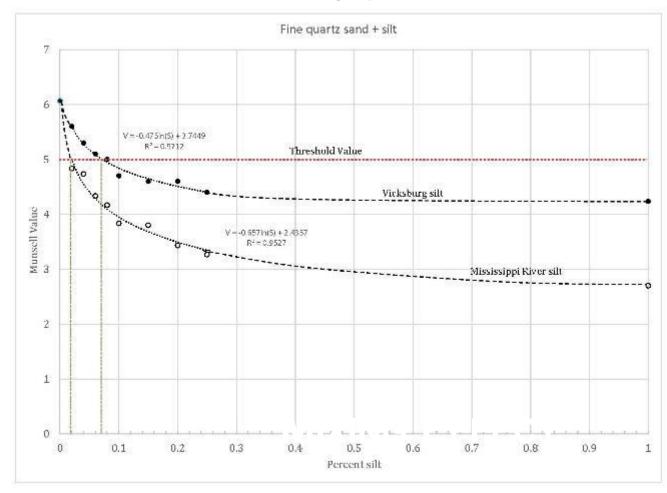


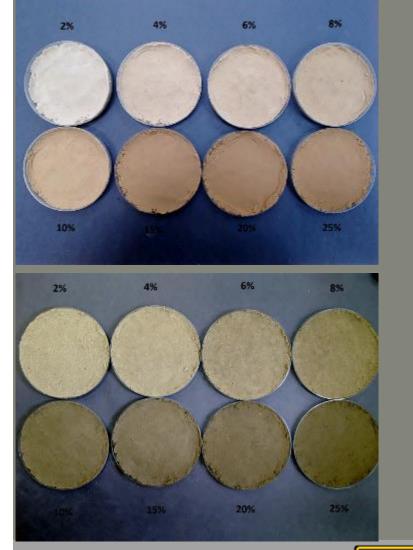




### **DOES SILT DECREASE MUNSELL COLOR VALUE?** <sup>24</sup>

Addition of 2-5% fines resulted in darkening beyond established color thresholds











### **UV LIGHT INDUCED COLOR CHANGE**

Exposure to high intensity light resulted in color change within 4 weeks of exposure



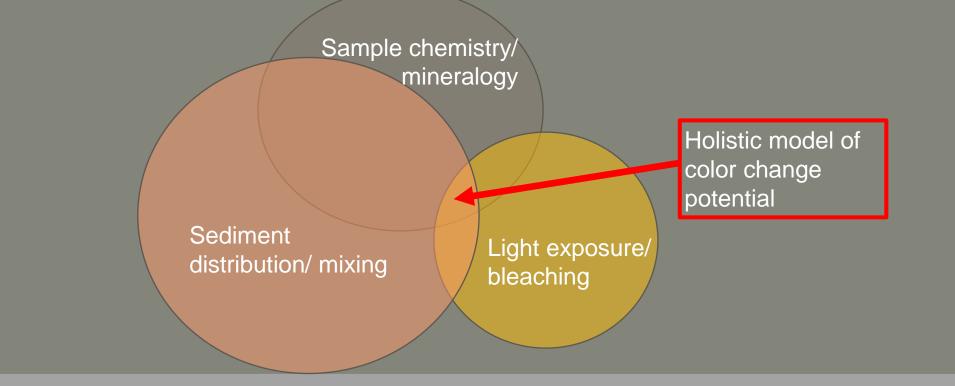






### **APPLIED R&D COLOR CHANGE PROPENSITY**

- 1. Synthesize bleaching, mixing, and chemistry effects into holistic model
- 2. Develop predictive guidance  $\rightarrow$  color change propensity







#### EMPIRICAL FORMULA TO ESTIMATE BORROW SEDIMENT ULTIMATE CAPABILITY

#### MAGLIO AND DAS FORMULA

#### Given

- Dredged sediment dramatically changes during the dredging and placement process
- Every dredge project is highly variable: in terms of its operations
- Formula non-dimensional
- Based on previous work and field observations
  - A few key parameters appear to control sediment changes
  - Number of times material was slurried (washed)
  - Slope of the discharged return water channel on the beach (velocity)
  - Sediment fall velocity (sedimentation)
    - Specific gravity
    - Size of particle
    - Shape factor
    - Salinity
    - Temperature





#### MAGLIO AND DAS FORMULA FOR EMPIRICAL DREDGED SEDIMENT CHANGE

% Loss = 
$$\sqrt{X}e^{(-10(2\sigma - 1)\sqrt{RS})}$$

X = No. of times sediment slurried

S = Berm Slope

R = Shape Factor adj. Particle Reynolds No. = Rep \* Z , for sphere, Z = 1

> $R_{ep} = (1 + 0.222 \frac{(S-1)gd^3}{16u^2})^{0.5}$ -1 S = Specific Gravity of sediment v = Kinematic viscosity of water (m<sup>2</sup>/s) d = Nominal diameter (m) g = acceleration of gravity =  $9.81 \text{ m/s}^2$ Z = Shape Factor Adjustment (Fitted) = [0.16 ln(d) +1.7] \* SF SF = Shape factor (0.3 to 1.0)

 $\sigma$  = sediment sorting parameter

$$\sigma = \frac{\phi_{84} - \varphi_{16}}{4} + \frac{\phi_{95} - \varphi_5}{6.6}$$

 $\sigma < 0.5$  (Well sorted);  $\sigma = 0.5 - 1.0$  (Moderately sorted);  $\sigma = 1 - 2$  (*Poorly sorted*);

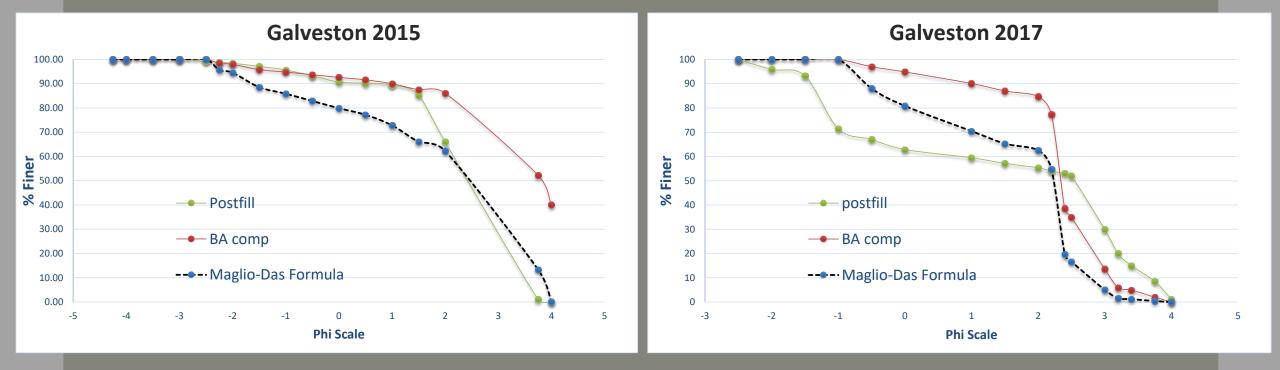




of Engineers

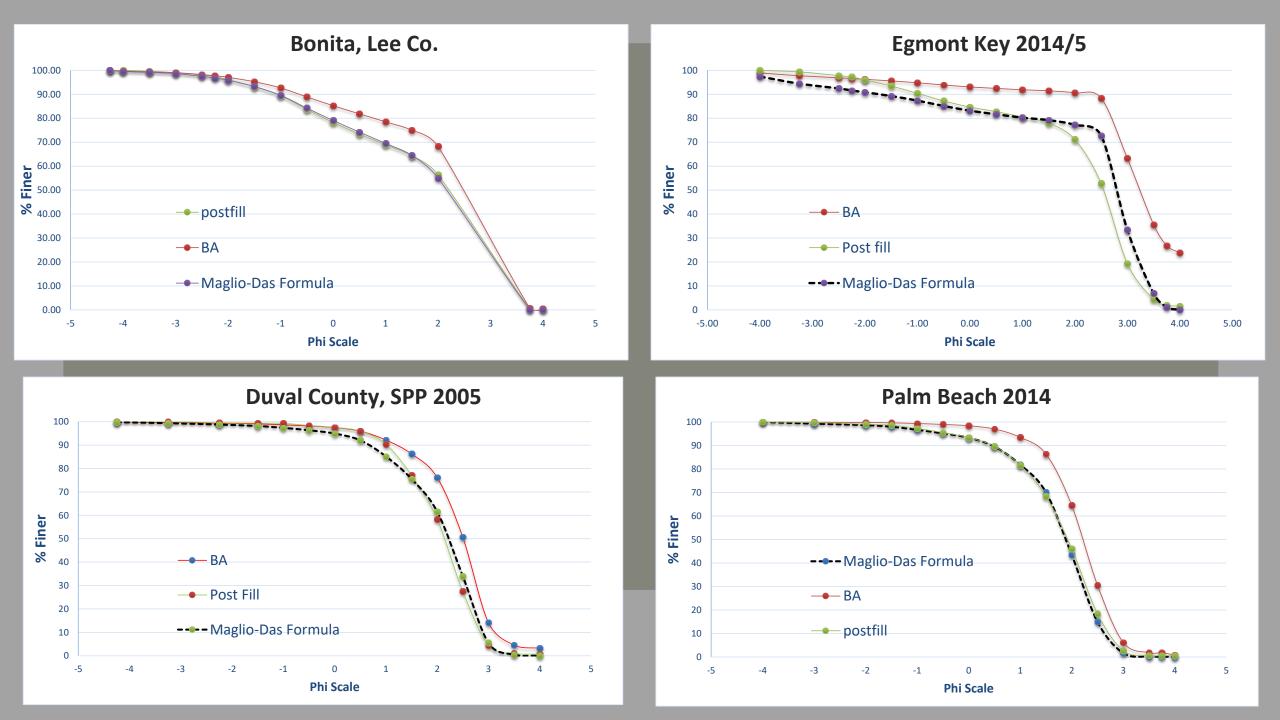
#### MAGLIO AND DAS FORMULA FOR EMPIRICAL DREDGED SEDIMENT CHANGE

% Loss =  $\sqrt{X}e^{(10(1-2\sigma)\sqrt{RS})}$ 



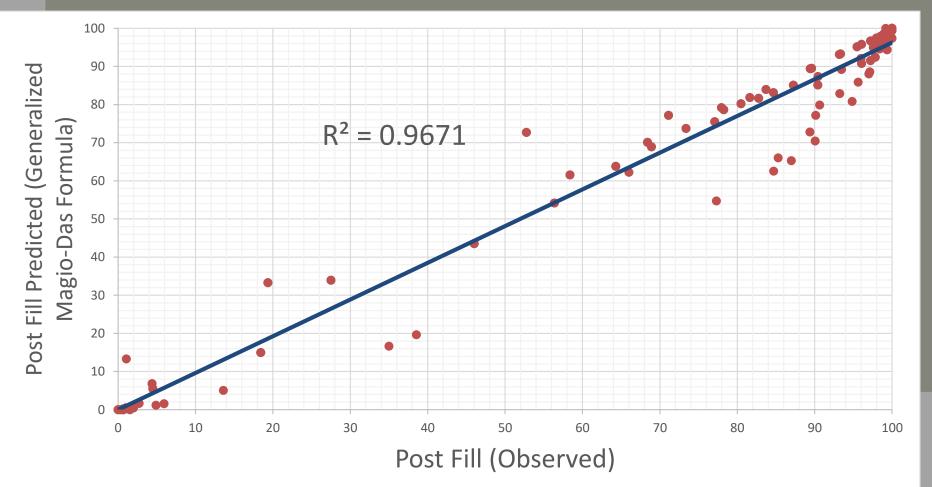






#### EMPIRICAL FORMULA TO ESTIMATE SEDIMENT CAPABILITY

# MAGLIO AND DAS FORMULA % LOSS = $\sqrt{X}e^{(-10(2\sigma-1)\sqrt{RS})}$



- Next step Beaches and Shores Article
- Conduct sensitivity analysis of factors
- Provide data to peers for validation
- Journal publication





### SUMMARY AND CONCLUSIONS

#### **Sediment Sampling**

- Grain Size indicates significant "fines" losses during dredging process
  - If allowed for in operations
- Fine material post-placement located at the toe of the fill
  - Mobilized during high energy events
- Munsell Color similar to pre-conditions
- Compaction similar to pre-conditions

#### **Predictive Capabilities**

- ERDC working on sediment color change potential, 3<sup>rd</sup> year, to assist BU acceptance
- Maglio-Das empirical formula appears to have significant promise





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